Investigation of wear behavior for novel polyamide 66 composites under dry sliding conditions

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Abstract
Polyamide 66 has been recently used in mechanical applications especially in gears manufacturing due to their low weight, low cost, and good tribological characteristics. In particular, a great attention must be considered on the specific wear rate for polyamide 66 and their composites under dry sliding conditions. The goal of this paper is to study the effect of wear parameters; applied load, sliding distance and thermal effects on specific wear rate for neat polyamide 66 and their composites after adding 1% wt CNT or 30%wt (CF) under dry sliding conditions as well as, study the effect of the reinforcement materials on the hardness and their relationship to specific wear rate. The experimental result shows that the increasing in wear parameters leads to increase the specific wear rate. However, with the addition of 1% wt CNT or 30%wt (CF) increasing the wear resistance by 130% and 200% under (30N) applied load and by 107% and 144% under (4000m) sliding distance respectively moreover, significant increasing in hardness explained the enhancement in wear resistance. A scanning electron microscopy was done for the harmed specimen surfaces and the images appeared that the addition of reinforcement materials give smooth surfaces with little harm unlike neat polyamide 66.

KEYWORDS: polyamide 66; CNT; carbon fibers; specific wear rate; hardness.

1. Introduction
Polymer and their composites become a very important material in manufacturing of mechanical parts especially at recent years, which replaced metallic parts in many tribological applications due to their easily manufacturing, low weight, low cost as well as their excellent wear and corrosion resistant [1]. Polyamide 66 or as known nylon 66 is a new version of polyamides group it attract attention recently due to their unique properties such as high mechanical strength, rigidity, good wear resistant and good stability under thermal and chemical effect [2]. Since polymer and their composites have been used widely in sliding application this necessitate understanding the wear behavior and mechanisms under variant sliding conditions [3].
Various researchers investigated the effect of adding fibers and nano particles as a reinforcement material to polymers and their effect on tribological characteristics. H. Meng et al. [4] studies the effect of adding 1%wt of carbon nanotube (CNT) as a reinforcement material to polyamide 6 on wear behavior. They observed that the use of CNT as a reinforcement material leads to increase the wear resistance due to generate transfer film between the pin and disc which is work as a self-lubricant between the meeting surfaces. J. Li and Y. C. Xia [5] investigated the wear behavior for polyamide 6 and their composites after adding CF with (10, 20, and 30 Vol%), the results show an increment in wear resistance up to 20% addition and after that was decreased. A. M. E. Eleiche et al. [6] suggested a new polyamide 66 composite reinforced by 2% glass fiber (GF), 1% MoS2, and 0.7% Mica platelets to overcome the tribological problems in rotating bands, the results appeared that the suggested composite has combination of strength, wear and heat resistance, as well as structural stability during service. S. M. Lee et al. [7] investigated the effect of CNT length with 1%wt used as a reinforcement material to polyamide 66 on tribological properties. The results indicate that the long CNT addition give better wear resistances than short and medium CNT as well as, long CNT decrease the wear rate under range of temperatures up to 110 °C after that will be increased. Kei Shibata et al. [8] studies the wear behavior for polyamide 66 (PA66) reinforced by rice bran ceramics (RBC) particles at wide range of pressure-velocity (PV) values under dry conditions. The results show reduction in specific wear rate with the addition various weight fractions of RBC particles to PA66 by (55-86%) in compared with pure polyamide 66. M. M. Sakka et al. [9] studies the influence of carbon nanotube and graphite fillers in epoxy resin on wear behavior, the results indicate that the addition of 1.5% CNT present a great improvement in wear resistance. Guglani and Gupta [10] studies the effect of adding micro titanium dioxide with different weight fraction to polyamide 66 on wear behavior under different parameters. They concluded that the addition of micro TiO2 to polyamide 66 up to 6 wt% leads to reduce wear rate and they suggested using combination from 2 wt% to 6 wt% micro titanium dioxide with polyamide 66 for best performance in applications that need good tribological properties.

In the present work the effect of different parameters such as applied load, sliding distance and elevated temperatures on specific wear rate of polyamide 66 and their composites were investigated after adding 1% wt CNT or 30% wt CF under dry sliding conditions as well as, study the effect of the reinforcement materials on the hardness and their relationship to specific wear rate.

2. Experimental details
2.1. Materials

Polyamide 66 and their composites with 1% wt CNT or 30% wt CF were obtained from Guangzhou engineering plastic industries (group) Co., Ltd., were used to prepared wear and hardness test specimens.

2.2. Composite preparation

The composites were prepared by injection polyamide 66 with 1% CNT (purity => 95%, diameter: 20-25 nm, length: 25-40 μm) or 30% CF with (diameter: 10 μm, average length 260 μm) in rod shape with 120mm diameter and 750mm length.

2.3. Experimental tests
2.3.1. Wear test

Wear test for polyamide 66 and their composites were carried out by pin-on-disc tribometer shown in Figure (1) in order to
estimate the specific wear rate for the composite specimens prepared according to ASTM G99-05 under dry sliding condition [11]. Cylindrical specimen pin (10 mm diameter and 20 mm length) and stainless steel disc (AISI 314) with surface roughness 0.25-0.3 and 0.15 µm respectively were prepared for this purpose. On the other hand to investigated the thermal effect on wear behaviour a small furnace with suitable dimensions was added to tribometer including (2000 watt) electrical heater fixed inside and K-type thermocouple used to control the internal temperature while the furnace outside was insulated with two layers of woven glass fiber to prevent heat leakage. The electrical furnace was connected to digital thermal control unit board in order to select the testing temperature.

Figure (1): Schematic representation of pin-on-disc tribometer.

The test was carried out at a rotating speed 300 rpm, applied loads from 5 N to 30 N, variant sliding distances from 0.6 up to 4 km and range of temperatures from room temperature to 130 °C. After the tests, the specimens cleaned and weighed by electrical balance (Radwag AS 160/C/2 with accuracy 0.0001g). For more accuracy three tests were carried out under each test condition and the average values of specimen weight were used for further analysis. Scanning electron microscopy (SEM) was carried out for specimen surfaces in order to obtain more information about the wear mechanism under the effect of applied load at room temperature (T_R) and 130 °C. The specific wear rate (S.W.R) was calculated by equation (1).

$$S.W.R = \frac{(\Delta m * 1000)}{(\rho * W * X)}$$

Where $\Delta m$ the mass loss of the specimen (g), $\rho$ is the specimen density (g/cm$^3$), $W$ is the normal load in (N), and $X$ is the sliding distance (m). Sliding distance $X$ calculated by equation (2).

$$X = \pi*D*n*t$$

Where D is the disc diameter (m), $n$ is the rotational speed of disc (rpm), and $t$ is the sliding time in (min) [2, 4].

2.3.2. Hardness test

Hardness test was carried out for polyamide 66 and their composites by shore D hardness tester analogue DIN 53505 (Germany). A load of (44.64 N) was applied on the specimens, at least ten data was calculated to find the hardness for each specimen.

3. Results and discussion

3.1. Hardness test

The variation in hardness of neat polyamide 66 and their composites shown in figure (2), it can be seen that the addition of 1% CNT or 30% CF to polyamide 66 leads to significant increasing in hardness. The results showed that the composite material prepared from polyamide 66 with 30%wt CF has higher hardness value than PA66/1%CNT composite due to the greater surface area of CF which in contact with polyamide 66 than CNT made the first composite has higher bonding and will be harder.
3.2. Wear test

The variation in specific wear rate of polyamide 66 and their composites with various applied loads, sliding distances, and temperatures under dry sliding conditions are considered in this test.

3.2.1. Applied load effect

The specific wear rate of polyamide 66 and their composites with the increasing in applied normal loads are shown in figure (3). It can be seen that the specific wear rate of polyamide 66 composites always have lower value than neat polyamide 66 under the same sliding conditions, which indicated that the addition of reinforcement materials leads to improve the wear resistance.

3.2.2. Sliding distance effect

The effect of sliding distances on polyamide 66 and their composites was carried out under constant applied load equal to (30N). Figure (4) presents the variation in the specific wear rate of polyamide 66 and their composites under variant sliding distances. It can be observed that the wear resistance of polyamide 66 composites always higher than neat polyamide 66 under the same test conditions, which indicated that the addition of reinforcement materials leads to reduce the specific wear rate.
The increasing in sliding distance leads to increase the specific wear rate of polyamide 66 and their composites. As shown above the addition of (1% CNT or 30% CF) leads to a great enhancement in wear resistance by (107% and 144%) respectively under longest sliding distance (4 km), this enhancement was due to the strong bonding between the matrix and the reinforcement material which will be generated a transfer films between the specimen and the disc worked to prevent the polyamide 66 composites from the hard metal asperities.

3.2.3. Thermal effect
The wear rate of polyamide 66 and their composites was tested as a function of temperature, which was examined at constant applied load and sliding distance equal to (30 N and 4000 m) respectively.

To obtain approximately complete perception in wear behaviour for polymers under thermal effect it should be specify the glass transition temperature (T_g) in order to compare the wear behaviour before and after this temperature. Differential scanning calorimetry (DSC) test has been done to specify the T_g for polymer composites used in this research, the results appeared that the T_g for polyamide 66 and their composites approximately (50°C) and this value has a great agreement with [7, 12]. Based on this result the investigation of thermal effect on wear behaviour was done from room temperature up to 130 °C in order to get as possible the general influence of temperature on wear behaviour for polyamide 66 and their composites.

Figure (5) appeared the specific wear rate behaviour of polyamide 66 and their composites before and after T_g. It can be seen that the increasing in temperature from room temperature up to 50°C leads to uniform increasing in specific wear rate as well as the polyamide 66 composites have better wear resistance than neat polyamide 66 under the same test conditions.

Figure (5): effect of temperature on specific wear rate.

Just crossing T_g an explicit increasing in specific wear rate specially in neat polyamide 66 can be seen, but near 90°C a sharp increasing will happened due to the softening in polyamide 66 asperities. In contrast polyamide 66 composites have the same behaviour of neat polyamide 66 in range of temperatures below T_g but with the increasing in temperature up to 130°C gradually increasing will happened in specific wear rate which means that the addition of the (1%CNT or 30%CF) help to minimize the thermal effect as possible and prevent polyamide 66 from softening with reduction in specific wear rate by (77% and 116%) respectively.

3.3. Scanning electron microscopy
For more information about the wear mechanism that is generated due to the applied load before and after T_g scanning electron microscopy (SEM) test was done on sliding surfaces of the pin specimens as shown in figure (6). The harmed surfaces for polyamide 66 and their composites before T_g was showed in Figures (a to c) while the figures (d to f) display the harmed surfaces after T_g.
Figure (6): SEM images of the typical harm surfaces of (a) PA66 at 25°C, (b) PA66+CNT

Note: Accepted manuscripts are articles that have been peer-reviewed and accepted for publication by the Editorial Board. These articles have not yet been copyedited and/or formatted in the journal house style.
at 25°C, (c) PA66+CF at 25°C, (d) PA66 at 130°C, (e) PA66+CNT at 130°C, and (f) PA66+CF at 130°C.

As shown in figure (6-a) the normal applied load leads to harm in polyamide 66 specimen surface displaying as adhesive marks in the direction of sliding with a small detachment of particles appeared as a groove in the contact surface, in contrast a considerable reduction in harm and adhesion due to employing of CNT or CF in polyamide 66 as appeared in figures (b & c). A relatively smooth surfaces and a few adhesive marks was found which indicates the addition of nano particle or the reinforcing fibers improved wear resistance of the composite. Both CF and CNT particles serves as a solid lubricant to prohibit the direct contact between the meeting surfaces. This observation was compatible with the fact that the addition of reinforcement materials made the composites harder and better resistance to detachment when sliding against the steel disc surface.

One of the most important necessities was conceive the wear mechanism of polyamide 66 and their composites at range of temperatures above T_g and considered their surface attitude under dry sliding conditions. As shown in figure (6-d) the neat polyamide 66 suffered high wear rate when served under (130 °C) and applied load equal to (30N). The first significance can be noticed was the appearance of ploughed marks in sliding direction and that indicated an abrasive wear mechanism that happened as well as, a softening occurred in the contact zone leads to a rough harm surface. On the other hand, the polyamide 66 composites appeared different behaviour under the same test conditions as shown in figure (e& f) the CNT particles leads to smooth surfaces with some narrow strips parallel to the sliding direction can by classified as adhesive marks and that classification have a great corroborate with behavior of CNT/polyamide 66 composite sliding at elevated temperature in contract, the employing of CF in polyamide 66 appeared the best performance at elevated temperatures due to the enhancement in structural strength which leads to high resistance results from strong bonding between the matrix and fiber as well as, the generation of transfer film at contact zone minimized the wear rate as possible and give smoother surface with little adhesive marks.

4. Conclusions
From the tribological study on polyamide 66 and their composites, the following conclusions can be obtained:
1- The addition of CNT and CF afford higher hardness values for polyamide 66 composites than neat polyamide 66.
2- The increasing in wear test parameters; applied load, sliding distance and temperature leads to increase the specific wear rate for neat polyamide 66 and their composites by variant percentage.
3- In spite of increasing in applied load, sliding distance and temperature the addition of 1% CNT or 30% CF reduce the increasing in specific wear rate with great reduction percentage in comparison with neat polyamide 66 under same test conditions.
4- A little uniform increasing in specific wear rate was happened for polyamide 66 and their composites before the T_g while, a rapid increasing in neat polyamide 66 was seen after T_g with a steady state increasing for their composites due to the addition of reinforcing materials.
5- From the above results the addition of 30%wt of CF to polyamide 66 gives the highest wear resistance and hardness under all the test conditions.
References


